

1. BASIC CALCULATIONS

Required bearing size is determined by the action of the external forces and according to the bearing required life and its reliability in the arrangement. Magnitude, direction and kind of load acting on the bearing, as well as the operating speed, are decisive for the type and bearing size selection. Other special or important conditions of each individual arrangement must be taken into account, e.g. operating temperature, limited space availability, simplicity of mounting, lubrication requirements, sealing, etc., and all of these can influence selection of the most suitable bearing. For given concrete conditions various bearing types can meet those requirements.

From the point of view of outer load acting and the bearing function in respective arrangement or unit we distinguish two types of the rolling bearing load in the bearing technique :

- when rolling bearing rings are relatively rotating against each other and bearing is under outer load (which is valid for most bearings), this is called *dynamic bearing load*,
- when rolling bearing rings either do not move against each other or they move only very slowly, the bearing carries an oscillating motion or the outer load acts for a shorter time than one bearing revolution, this is called *static bearing load*.

For bearing safety calculation, the life limited by bearing breakdown due to material fatigue of a bearing component is decisive in the first case. In the second case there are durable deformations of functional surfaces on the contact surfaces of rolling elements and raceways.

1.1 DYNAMIC LOAD

1.1.1 Basic Dynamic Load Rating

Basic dynamic load rating is a constant invariable load which the bearing can theoretically carry at the nominal life of one million revolutions. For radial bearings, the radial dynamic load rating C_r refers to constant load. For thrust bearings, the axial dynamic load rating C_a refers to unvariable, purely axial load, acting centrally.

Basic dynamic load ratings C_r and C_a , whose size depends on bearing dimensions, rolling element number, material and bearing design, are shown for each bearing in the dimension tables. Values of the basic dynamic load ratings were stated according to the standard ISO 281. These values are verified in testing equipments and by operation results.

1.1.2 Life

Rolling bearing life is defined as the number of revolution carried out by one bearing ring against the other ring, until the first signs of material fatigue occur on one ring or the rolling element. Great differences in life can occur among bearings of the same type, that is why according to the standard STN ISO 281 the basic life is used as the basis for life calculation, i.e. life shown by the operation time attained or exceeded by a bearing group at 90% reliability.

Life Equation

Nominal bearing life is mathematically defined by the life equation valid for all bearing types.

$$L_{10} = \left(\frac{C}{P} \right)^p \quad \text{or} \quad \frac{C}{P} = \left(L_{10} \right)^{\frac{1}{p}}$$

L_{10}	- nominal life	[10 ⁶ rev]
C	- basic dynamic load rating (values C_r , C_a are given in the dimension tables)	[kN]
P	- equivalent dynamic bearing load (equations for P_r , P_a calculations are in section 1.1.3 and at each design group of bearings)	[kN]

p - exponent: for ball bearings
for cylindrical, needle-, spherical- and tapered roller bearings

p = 3
p = 10 / 3

Table 1 shows dependence of the life L_{10} in million revolutions and respective ratio C/P.
If the rotational speed does not change, the revised life calculation expressing the nominal life in operation hours can be used:

$$L_{10h} = \left(\frac{C}{P} \right)^p \cdot \frac{10^6}{60 \cdot n}$$

L_{10h} - nominal life

n - rotational speed

[h]
[min⁻¹]

C/P dependence from the nominal life L_{10} and the rotational speed n is shown for ball bearings in Table 2, for cylindrical roller, needle roller, spherical roller and tapered roller bearings in Table 3.

C/P ratio in dependence on life L_{10h}							Table 1
For ball bearings				For cylindrical roller, needle roller, spherical roller and tapered roller bearings			
Life	C/P	Life	C/P	Life	C/P	Life	C/P
L_{10}		L_{10}		L_{10}		L_{10}	
10 ⁶	rev	10 ⁶	rev	10 ⁶	rev	10 ⁶	rev
0,5	0,793	600	8,43	0,5	0,812	600	6,81
0,75	0,909	650	8,66	0,75	0,917	650	6,98
1	1	700	8,88	1	1	700	7,14
1,5	1,14	750	9,09	1,5	1,13	750	7,29
2	1,26	800	9,28	2	1,24	800	7,43
3	1,44	850	9,47	3	1,39	850	7,56
4	1,59	900	9,65	4	1,52	900	7,70
5	1,71	950	9,83	5	1,62	950	7,82
6	1,82	1000	10	6	1,71	1000	7,94
8	2	1100	10,3	8	1,87	1100	8,17
10	2,15	1200	10,6	10	2	1200	8,39
12	2,29	1300	10,9	12	2,11	1300	8,59
14	2,41	1400	11,2	14	2,21	1400	8,79
16	2,52	1500	11,4	16	2,30	1500	8,97
18	2,62	1600	11,7	18	2,38	1600	9,15
20	2,71	1700	11,9	20	2,46	1700	9,31
25	2,92	1800	12,2	25	2,63	1800	9,48
30	3,11	1900	12,4	30	2,77	1900	9,63
35	3,27	2000	12,6	35	2,91	2000	9,78
40	3,42	2200	13	40	3,02	2200	10,1
45	3,56	2400	13,4	45	3,13	2400	10,3
50	3,68	2600	13,8	50	3,23	2600	10,6
60	3,91	2800	14,1	60	3,42	2800	10,8
70	4,12	3000	14,4	70	3,58	3000	11
80	4,31	3500	15,2	80	3,72	3500	11,5
90	4,48	4000	15,9	90	3,86	4000	12
100	4,64	4500	16,5	100	3,98	4500	12,5
120	4,93	5000	17,1	120	4,20	5000	12,9
140	5,19	5500	17,7	140	4,40	5500	13,2

C/P ratio in dependence on life L_{10h}							Table 1
For ball bearings				For cylindrical roller, needle roller, spherical roller and tapered roller bearings			
Life	C/P	Life	C/P	Life	C/P	Life	C/P
L_{10}		L_{10}		L_{10}		L_{10}	
10^6	rev	10^6	rev	10^6	rev	10^6	rev
160	5,43	6000	18,2	160	4,58	6000	13,6
180	5,65	7000	19,1	180	4,75	7000	14,2
200	5,85	8000	20	200	4,90	8000	14,8
250	6,30	9000	20,8	250	5,24	9000	15,4
300	6,69	10000	21,5	300	5,54	10000	15,8
350	7,05	12500	23,2	350	5,80	12500	16,9
400	7,37	15000	24,7	400	6,03	15000	17,9
450	7,66	17500	26	450	6,25	17500	18,7
500	7,94	20000	27,1	500	6,45	20000	19,5
550	8,19	25000	29,2	550	6,64	25000	20,9

C/P ratio in dependence on life L_{10h} and rotational speed n for ball bearings														Table 2
Life	Rotational speed n [min^{-1}]													
L_{10h}	10	16	25	40	63	100	125	160	200	250	320	400	500	630
h														
100	-	-	-	-	-	-	-	-	1,06	1,15	1,24	1,34	1,45	1,56
500	-	-	-	1,06	1,24	1,45	1,56	1,68	1,82	1,96	2,12	2,29	2,47	2,67
1 000	-	-	1,15	1,34	1,56	1,82	1,96	2,12	2,29	2,47	2,67	2,88	3,11	3,36
1 250	-	1,06	1,24	1,45	1,68	1,96	2,12	2,29	2,47	2,67	2,88	3,11	3,36	3,63
1 600	-	1,15	1,34	1,56	1,82	2,12	2,29	2,47	2,67	2,88	3,11	3,36	3,63	3,91
2 000	1,06	1,24	1,45	1,68	1,96	2,29	2,47	2,67	2,88	3,11	3,36	3,63	3,91	4,23
2 500	1,15	1,34	1,56	1,82	2,12	2,47	2,67	2,88	3,11	3,36	3,63	3,91	4,23	2,56
3 200	1,24	1,45	1,68	1,96	2,29	2,67	2,88	3,11	3,36	3,63	3,91	4,23	4,56	4,93
4 000	1,34	1,56	1,82	2,12	2,47	2,88	3,11	3,36	3,63	3,91	4,23	4,56	4,93	5,32
5 000	1,45	1,68	1,96	2,29	2,67	3,11	3,36	3,63	3,91	4,23	4,56	4,93	5,32	5,75
6 300	1,56	1,82	2,12	2,47	2,88	3,36	3,63	3,91	4,23	4,56	4,93	5,32	5,75	6,20
8 000	1,68	1,96	2,29	2,67	3,11	3,63	3,91	4,23	4,56	4,93	5,32	5,75	6,20	2,70
10 000	1,82	2,12	2,47	2,88	3,36	3,91	4,23	4,56	4,93	5,32	5,75	6,20	6,70	7,23
12 500	1,96	2,29	2,67	3,11	3,36	4,23	4,56	4,93	5,32	5,75	6,20	6,70	7,23	7,81
16 000	2,12	2,47	2,88	3,36	3,91	4,56	4,93	5,23	5,75	6,20	6,70	7,23	7,81	8,43
20 000	2,29	2,67	3,11	3,63	4,23	4,93	5,32	5,75	6,20	6,70	7,23	7,81	8,43	9,11
25 000	2,47	2,88	3,36	3,91	4,56	5,32	5,75	6,20	6,70	7,23	7,81	8,43	9,11	9,83
32 000	2,67	3,11	3,63	4,23	4,93	5,75	6,20	6,70	7,23	7,81	8,43	9,11	9,83	10,6
40 000	2,88	3,36	3,91	4,56	5,32	6,20	6,70	7,23	7,81	8,43	9,11	9,83	10,6	11,5
50 000	3,11	3,63	4,23	4,93	5,75	6,70	7,23	7,81	8,43	9,11	3,83	10,6	11,5	12,4
63 000	3,36	3,91	4,56	5,32	6,20	7,23	7,81	8,43	9,11	9,83	10,6	11,5	12,4	13,4
80 000	3,36	4,23	4,93	5,75	6,70	7,81	8,43	9,11	9,83	10,6	11,5	12,4	13,4	14,5
100 000	3,91	4,56	5,32	6,20	7,23	8,43	9,11	9,83	10,6	11,5	12,4	13,4	14,5	15,6
200 000	4,93	5,75	6,70	7,81	9,11	10,6	11,5	12,4	13,4	14,5	15,6	16,8	18,2	19,6



C/P ratio in dependence on life L_{10h} and rotational speed n for ball bearings

Table 2

Life	Rotational speed n [min ⁻¹]													
	L_{10h}	800	1000	1250	1600	2000	2500	3200	4000	5000	6300	8000	10000	12500
h														
100	1,68	1,82	1,96	2,12	2,29	2,47	2,67	2,88	3,11	3,36	3,63	3,91	4,23	4,56
500	2,88	3,11	3,36	3,63	3,91	4,23	4,56	4,93	5,32	5,75	6,2	6,7	7,23	7,81
1 000	3,63	3,91	4,23	4,56	4,93	5,32	5,75	6,20	6,70	7,23	7,81	8,43	9,11	9,83
1 250	3,91	4,23	4,56	4,93	5,32	5,75	6,20	6,70	7,23	7,81	8,43	9,11	9,83	10,6
1 600	4,23	4,56	4,93	5,32	5,75	6,20	6,70	7,23	7,81	8,43	9,11	9,83	10,6	11,5
2 000	4,56	4,93	5,32	5,75	6,20	6,70	7,23	7,81	8,43	9,11	9,83	10,6	11,5	12,4
2 500	4,93	5,32	5,75	6,20	6,70	7,23	7,81	8,43	9,11	9,83	10,6	11,5	12,4	13,4
3 200	5,32	5,75	6,20	6,70	7,23	7,81	8,43	9,11	9,83	10,6	11,5	12,4	13,4	14,5
4 000	5,75	6,20	6,70	7,23	7,81	8,43	9,11	9,83	10,6	11,5	12,4	13,4	14,5	15,6
5 000	6,20	6,70	7,23	7,81	8,43	9,11	9,83	10,6	11,5	12,4	13,4	14,5	15,6	16,8
6 300	6,70	7,23	7,81	8,43	9,11	9,83	10,6	11,5	12,4	13,4	14,5	15,6	16,8	18,2
8 000	7,23	7,81	8,43	9,11	9,83	10,6	11,5	12,4	13,4	14,5	15,6	16,8	18,2	19,6
10 000	7,81	8,43	9,11	9,83	10,6	11,5	12,4	13,4	14,5	15,6	16,8	18,2	19,6	21,2
12 500	8,43	9,11	9,83	10,6	11,5	12,4	13,4	14,5	15,6	16,8	18,2	19,6	21,2	22,9
16 000	9,11	9,83	10,6	11,5	12,4	13,4	14,5	15,6	16,8	18,2	19,6	21,2	22,9	24,7
20 000	9,83	10,6	11,5	12,4	13,4	14,5	15,6	16,8	18,2	19,6	21,2	22,9	24,7	26,7
25 000	10,6	11,5	12,4	13,4	14,5	15,6	16,8	18,2	19,6	21,2	22,9	24,7	26,7	28,8
32 000	11,5	12,4	13,4	14,5	15,6	16,8	18,2	19,6	21,2	22,9	24,7	26,7	28,8	31,1
40 000	12,4	13,4	14,5	15,6	16,8	18,2	19,6	21,2	22,9	24,7	26,7	28,8	31,1	-
50 000	13,4	14,5	15,6	16,8	18,2	19,6	21,2	22,9	24,7	26,7	28,8	31,1	-	-
63 000	14,5	15,6	16,8	18,2	19,6	21,2	22,9	24,7	26,7	28,8	31,1	-	-	-
80 000	15,6	16,8	18,2	19,6	21,2	22,9	24,7	26,7	28,8	31,1	-	-	-	-
100 000	16,8	18,2	19,6	21,2	22,9	24,7	26,7	28,8	31,1	-	-	-	-	-
200 000	21,2	22,9	24,7	26,7	28,8	31,1	-	-	-	-	-	-	-	-

C/P ratio in dependence on life L_{10h} and rotational speed n for cylindrical roller, spherical roller and tapered roller bearings Table 3

Life	Rotational speed n [min^{-1}]													
L_{10h}	10	16	25	40	63	100	125	160	200	250	320	400	500	630
h														
100	-	-	-	-	-	-	-	-	1,05	1,1	1,21	1,30	1,39	1,49
500	-	-	-	1,05	1,21	1,39	1,49	1,60	1,71	1,83	1,97	2,11	2,26	2,42
1 000	-	-	1,13	1,30	1,49	1,71	1,83	1,97	2,11	2,26	2,42	2,59	2,78	2,97
1 250	-	1,05	1,21	1,39	1,60	1,83	1,97	2,11	2,26	2,42	2,59	2,78	2,97	3,19
1 600	-	1,13	1,30	1,49	1,71	1,97	2,11	2,26	2,42	2,59	2,78	2,97	3,19	3,42
2 000	1,05	1,21	1,39	1,60	1,83	2,11	2,26	2,42	2,59	2,78	2,97	3,19	3,42	3,66
2 500	1,13	1,30	1,49	1,71	1,97	2,26	2,42	2,59	2,78	2,97	3,19	3,42	3,66	3,92
3 200	1,21	1,39	1,60	1,83	2,11	2,42	2,59	2,78	2,97	3,19	3,42	3,66	3,92	4,20
4 000	1,30	1,49	1,71	1,97	2,26	2,59	2,78	2,97	3,19	3,42	3,66	3,92	4,20	4,50
5 000	1,39	1,60	1,83	2,11	2,42	2,78	2,97	3,19	3,42	3,66	3,92	4,20	4,50	4,82
6 300	1,49	1,71	1,97	2,26	2,59	2,97	3,19	3,42	3,66	3,92	4,20	4,50	4,82	5,17
8 000	1,60	1,83	2,11	2,42	2,78	3,19	3,42	3,66	3,92	4,20	4,50	4,82	5,17	5,54
10 000	1,71	1,97	2,26	2,59	2,97	3,42	3,66	3,92	4,20	4,50	4,82	5,17	5,54	5,94
12 500	1,83	2,11	2,42	2,78	3,19	3,66	3,92	4,20	4,50	4,82	5,17	5,54	5,94	6,36
16 000	1,97	2,26	2,59	2,97	3,42	3,92	4,20	4,50	4,82	5,17	5,54	5,94	6,36	6,81
20 000	2,11	2,42	2,78	3,19	3,66	4,20	4,50	4,82	5,17	5,54	5,94	6,36	6,81	7,30
25 000	2,26	2,59	2,97	3,42	3,92	4,50	4,82	5,17	5,54	5,94	6,36	6,81	7,30	7,82
32 000	2,42	2,78	3,19	3,66	4,20	4,82	5,17	5,54	5,94	6,36	6,81	7,30	7,82	8,38
40 000	2,59	2,97	3,42	3,92	4,50	5,17	5,54	5,94	6,36	6,81	7,30	7,82	8,38	8,98
50 000	2,78	3,19	3,66	4,20	4,82	5,54	5,94	6,36	6,81	7,30	7,82	8,38	8,98	9,62
63 000	2,97	3,42	3,92	4,50	5,17	5,94	6,36	6,81	7,30	7,82	8,38	8,98	9,62	10,3
80 000	3,19	3,66	4,20	4,82	5,54	6,36	6,81	7,30	7,82	8,38	8,98	9,62	10,3	11,0
100 000	3,42	3,92	4,50	5,17	5,94	6,81	7,30	7,82	8,38	8,98	9,62	10,3	11,0	11,8
200 000	4,20	4,82	5,54	6,36	7,30	8,38	8,98	9,62	10,3	11,0	11,8	12,7	13,6	14,6

C/P ratio in dependence on life L_{10h} and rotational speed n for cylindrical roller, spherical roller and tapered roller bearings Table 3

Life	Rotational speed n [min^{-1}]													
L_{10h}	800	1000	1250	1600	2000	2500	3200	4000	5000	6300	8000	10000	12500	16000
h														
100	1,60	1,71	1,83	1,97	2,11	2,26	2,42	2,59	2,78	2,97	3,19	3,42	3,66	3,92
500	2,59	2,78	2,97	3,19	3,42	3,66	3,92	4,20	4,50	4,82	5,7	5,54	5,94	6,36
1 000	3,19	3,42	3,66	3,92	4,20	4,50	4,82	5,17	5,54	5,94	6,36	6,81	7,30	7,82
1 250	3,42	3,66	3,92	4,20	4,50	4,82	5,17	5,54	5,94	6,36	6,81	7,30	7,82	8,38
1 600	3,66	3,92	4,20	4,50	4,82	5,17	5,54	5,94	6,36	6,81	7,30	7,82	8,38	8,98
2 000	3,92	4,20	4,50	4,82	5,17	5,54	5,94	6,36	6,81	7,30	7,82	8,38	8,98	9,62
2 500	4,20	4,50	4,82	5,17	5,54	5,94	6,36	6,81	7,30	7,82	8,38	8,98	9,62	10,3
3 200	4,50	4,82	5,17	5,54	5,94	6,36	6,81	7,30	7,82	8,38	8,98	9,62	10,3	11,0
4 000	4,82	5,17	5,54	5,94	6,36	6,81	7,30	7,82	8,38	8,98	9,62	10,3	11,0	11,8
5 000	5,17	5,54	5,94	6,36	6,81	7,30	7,82	8,38	8,98	9,62	10,3	11,0	11,8	12,7
6 300	5,54	5,94	6,36	6,81	7,30	7,82	8,38	8,98	9,62	10,3	11,0	11,8	12,7	13,6
8 000	5,94	6,36	6,81	7,30	7,82	8,38	8,98	9,62	10,3	11,0	11,8	12,7	13,6	14,6
10 000	6,36	6,81	7,30	7,82	8,38	8,98	9,62	10,3	11,0	11,8	12,7	13,6	14,6	15,6
12 500	6,81	7,30	7,82	8,38	8,98	9,62	10,3	11,0	11,8	12,7	13,6	14,6	15,6	16,7
16 000	7,30	7,82	8,38	8,98	9,62	10,3	11,0	11,8	12,7	13,6	14,6	15,6	16,7	17,9
20 000	7,82	8,38	8,98	9,62	10,3	11,0	11,8	12,7	13,6	14,6	15,6	16,7	17,9	19,2
25 000	8,38	8,98	9,62	10,3	11,0	11,8	12,7	13,6	14,6	15,6	16,7	17,9	19,2	20,6
32 000	8,98	9,62	10,3	11,0	11,8	12,7	13,6	14,6	15,6	16,7	17,9	19,2	20,6	-
40 000	9,62	10,3	11,0	11,8	12,7	13,6	14,6	15,6	16,7	17,9	19,2	20,6	-	-
50 000	10,3	11,0	11,8	12,7	13,6	14,6	15,6	16,7	17,9	19,2	20,6	-	-	-
63 000	11,0	11,8	12,7	13,6	14,6	15,6	16,7	17,9	19,2	20,6	-	-	-	-
80 000	11,8	12,7	13,6	14,6	15,6	16,7	17,9	19,2	20,6	-	-	-	-	-
100 000	12,7	13,6	14,6	15,6	16,7	17,9	19,2	20,6	-	-	-	-	-	-
200 000	15,6	16,7	17,9	19,2	20,6	-	-	-	-	-	-	-	-	-

In arrangements of the axles of road and railway vehicles the nominal life can be expressed by a revised relation in the volume of kilometers travelled.

$$L_{10km} = \left(\frac{C}{P} \right)^p \cdot \frac{\pi \cdot D}{1000}$$

L_{10km} - nominal life
 D - wheel diameter

[10^6 km]
[m]

Reference Nominal Life Values

In cases, where the life for a given arrangement is not specified in advance, the values in tables 4 and 5 can be considered as adequate.

Reference Nominal Life Values in Operating Hours	Table 4
Machine Type	Nominal Life
	L_{10h}
	h
Devices and tools rarely used	1 000
Household electric appliances, small fans	2 000 to 4 000
Machines for intermittent operation, hand tools, workshop lifting tackles, agricultural machines	4 000 to 8 000
Machines with intermittent operation where high reliability is required, auxiliary power station equipment, belt conveyors, trucks, elevators	8 000 to 15 000
Rolling mills	6 000 to 12 000
Machines operating 8 - 16 hours - stationary electric motors, gear drives, textile machine spindles, plastic material processing machines, printing machines, cranes	15 000 to 30 000
Machine tools in general	20 000 to 30 000
Machines with continuous operation - stationary electric machines, conveying equipment, roller conveyors, pumps, centrifuges, blowers, compressors, hammer mills, crushers, briqueting presses, mine hoists, rope pulleys	40 000 to 60 000
Machines with continuous operation for high operating reliability - power station plants, water works machinery, paper making machines, ship machines	100 000 to 200 000

Reference Nominal Life Values in Kilometers	Table 5
Vehicle Type	Nominal Life
	L_{10km}
	km

Road vehicle wheels:

motor cycles	60 000
passenger cars	150 000 to 250 000
trucks, buses	400 000 to 500 000

Axle box bearings for railway vehicles:

freight wagons (according to UIC) under continuous maximum axle load acting	800 000
tram cars	1 500 000
railway passenger carriages	3 000 000
motor wagons and motor units	3 000 000 to 4 000 000
locomotives	3 000 000 to 5 000 000

Equation of Adjusted Life

Adjusted life is a corrected nominal life, where by calculation not only the load but the influence of bearing components, material, physical, mechanical, and chemical qualities of lubricants and the temperature regime of the bearing, the operating environment are taken into account.

$$L_{na} = a_1 \cdot a_{23} \cdot L_{10}$$

L_{na}	- adjusted life for (100-n)% reliability and other usual operation conditions	[10 ⁶ rev]
a_1	- life factor for other than 90% reliability, see Table 6	
a_{23}	- life factor of material, lubricant, production technology and operation conditions, see Pict. 1	
L_{10}	- nominal life	[10 ⁶ rev]

Factor a_1 Values		Table 6
Reliability (%)	L_n	a_1
90	L_{10}	1,00
95	L_5	0,62
96	L_4	0,53
97	L_3	0,44
98	L_2	0,33
99	L_1	0,21

We can find basic values of a_{23} by using the diagram in Figure 1.

$$K = \frac{\nu}{\nu_1}$$

ν	- kinematic lubricant viscosity by operation bearing temperature	[mm ² .s ⁻¹]
ν_1	- kinematic viscosity for defined rotational speed and selected bearing dimensions	[mm ² .s ⁻¹]

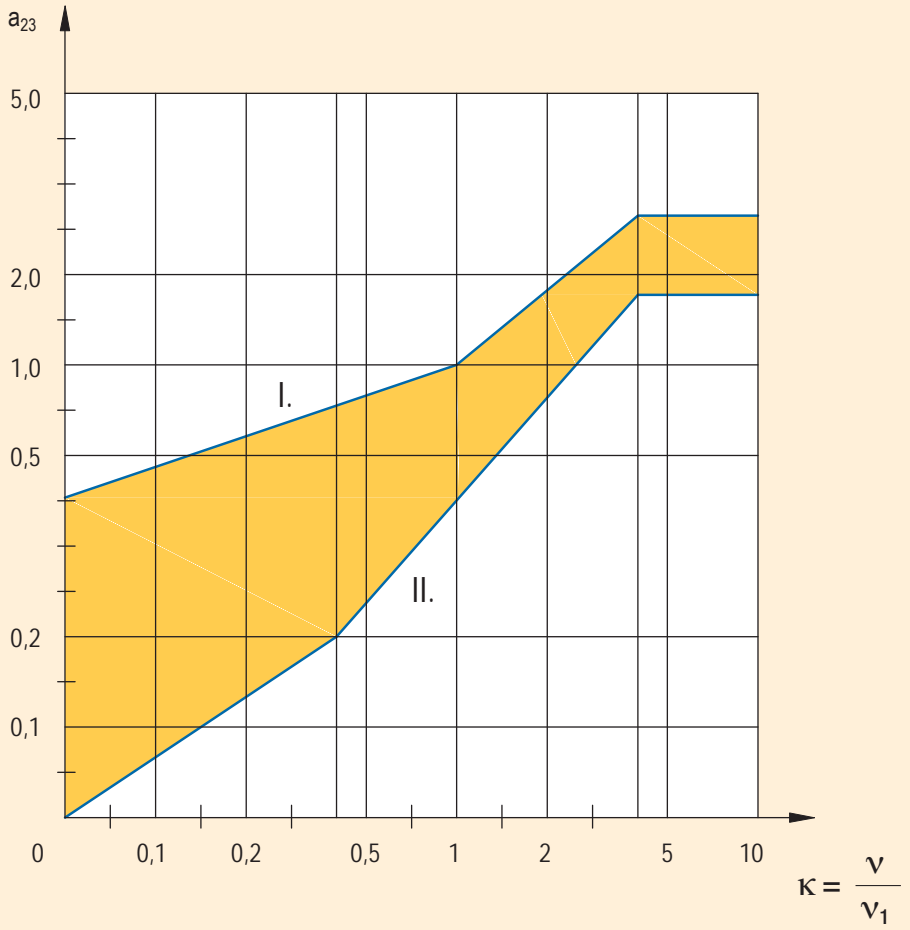
Values ν and ν_1 are determined according to the diagrams in Figure 23 or 24.

In the diagram, Figure 1, the line I is valid for radial ball bearings operating in a very clean environment. In other cases the factor a_{23} is lower, depending on the environment cleanliness, and the decreasing tendency is dependent on the bearing design group in following order :

- angular contact ball bearings
- tapered roller bearings
- cylindrical roller bearings
- double row self-aligning ball bearings
- spherical roller bearings

Line II can be used when stating the factor a_{23} for spherical roller bearings operating in a dusty environment.

We recommend consulting this issue with your supplier.



1.1.3 Equivalent Dynamic Load

In the arrangement the bearing is subjected to generally acting forces in various magnitudes, at various rotational speeds and with different acting period. From the point of view of calculation methodology the acting forces should be re-calculated into the constant load, by which the bearing will have the same life as it reaches in the conditions of the actual load. Such a re-calculated constant radial or axial load is called the equivalent load P , or P_r (radial) or P_a (axial).

Combined Load

Constant Load

The outer forces acting on a bearing are not changed both from the point of view of size and time dependence.

Radial Bearings

If the radial bearings are simultaneously subjected to constant forces in radial and axial directions, the following equation is valid for calculating the radial equivalent dynamic load:

$$P_r = X \cdot F_r + Y \cdot F_a$$

P_r	- radial equivalent dynamic load	[kN]
F_r	- radial bearing load	[kN]
F_a	- axial bearing load	[kN]
X	- radial load factor	
Y	- axial load factor	

Factors X and Y depend on the ratio F_a/F_r . Values X and Y are shown in the dimension tables or in the introduction to each bearing type where closer information regarding bearing calculation of the respective type is given.

Thrust Bearings

Thrust ball bearings can carry only forces acting in axial direction and the following equation is valid for calculating axial equivalent dynamic load:

$$P_a = F_a$$

P_a	- axial equivalent dynamic load	[kN]
F_a	- axial bearing load	[kN]

Spherical roller thrust bearings can also carry some radial load, but only by simultaneous acting of axial load, when condition $F_r \leq 0,55 F_a$ must be fulfilled. Axial equivalent dynamic load is calculated from equation

$$P_a = F_a + 1,2 \cdot F_r$$

Fluctuating Load

Real fluctuating load, whose time course we know, is for calculation replaced by mean hypothetical load. This hypothetical load has the same influence on the bearing as the fluctuating load.

Change of Load Magnitude by Constant Rotational Speed

If the bearing is subjected to a load in a constant direction, whose magnitude is changed in dependence on time and the rotational speed is constant (Figure 2), we can calculate the mean hypothetical load F_s according to the following equation

$$F_s = \left(\sum_{i=1}^n F_i^3 \cdot \frac{q_i}{100} \right)^{\frac{1}{3}}$$

F_s - mean hypothetical constant load [kN]
 $F_i = F_1, \dots, F_n$ - constant partial actual load [kN]
 $q_i = q_1, \dots, q_n$ - share of fractional load effects [%]

At constant rotational speed with linear change of the load in constant direction (see Figure 3) the mean hypothetical load can be calculated from equation

$$F_s = \frac{F_{\min} + 2 \cdot F_{\max}}{3}$$

Figure 2

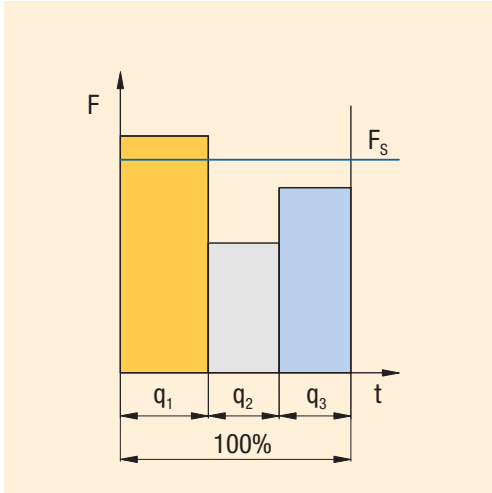
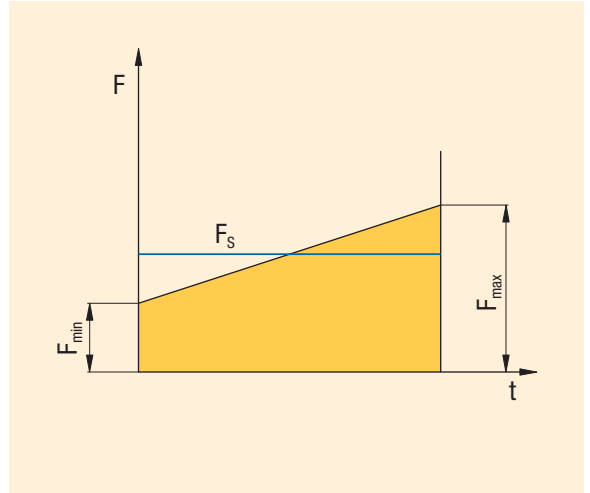


Figure 3



If the actual load has a sine behaviour (see Figure 4), the mean hypothetical load is

$$F_s = 0,75 \cdot F_{\max}$$

Change of Load Magnitude by Change of Rotational Speed

If the bearing is subjected in time to a varying load and the rotational speed is being changed, the mean hypothetical load is calculated from equation

$$F_s = \left(\frac{\sum_{i=1}^n F_i^3 \cdot q_i \cdot n_i}{\sum_{i=1}^n q_i \cdot n_i} \right)^{\frac{1}{3}}$$

$n_i = n_1, \dots, n_n$ - constant rotational speed in time of partial loads F_1, \dots, F_n acting [min⁻¹]
 $q_i = q_1, \dots, q_n$ - share of partial load and rotational speed acting [%]

If in dependence on time only the rotational speed is changed, the mean hypothetical constant rotational speed is calculated from equation

$$n_s = \frac{\sum_{i=1}^n q_i \cdot n_i}{100}$$

n_s = mean rotational speed [min⁻¹]

Figure 4

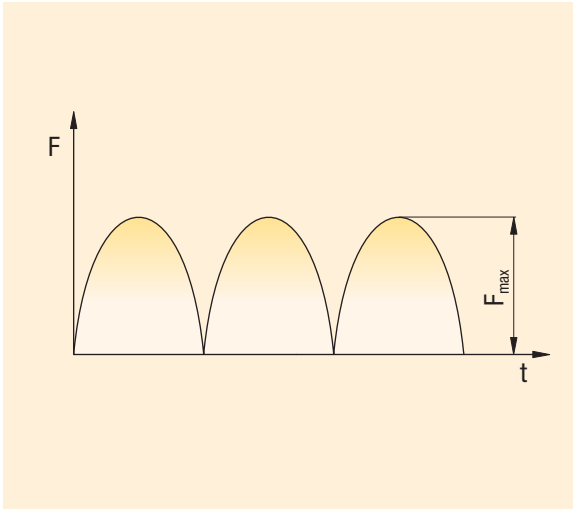
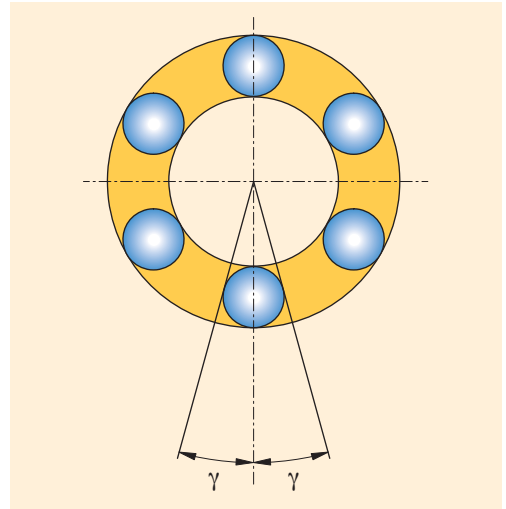


Figure 5



By oscillating motion with amplitude γ (see Figure 5) it is the simplest way of substituting the oscillating motion by hypothetical rotation, when the rotational speed equals the oscillation frequency. For radial bearings the mean hypothetical load is calculated from the equation:

$$F_s = F_r \left(\frac{\gamma}{90} \right)^{\frac{1}{p}}$$

- F_s - mean hypothetical load [kN]
- F_r - actual radial load [kN]
- γ - oscillating motion amplitude [°]
- p - exponent $p = 3$ for ball bearings
 $p = 10/3$ for cylindrical roller, needle roller, spherical roller and tapered roller bearings

1.1.4 Temperature Influence

Delivered bearing assortment is determined for usage in an environment with operating temperatures up to 120°C. Exceptions are double row spherical roller bearings which can work at temperatures up to 180°C, and single row ball bearings with seals (RS, 2RS, RSR, 2RSR, RSR2, -2RSR2) applicable up to 110°C, with seals RS2, -2RS2, RSR2, -2RSR2 applicable up to 180°C.

For higher operation temperatures the bearings are produced so that their necessary physical and mechanical qualities and dimensional stability can be secured.

Values of the basic dynamic load ratings C_r or C_a shown in the dimension tables of this publication should be multiplied by factor f_t , shown in Table 7.

Values of f_t Factor	Table 7			
Operating Temperature to [°C]	150	200	250	300
Factor f_t	0,95	0,9	0,75	0,6

1.2 STATIC LOAD

1.2.1 Basic Static Load Rating

Radial basic static load rating C_{or} and axial basic static load rating C_{oa} are shown for each bearing in the dimension tables of this publication. Values C_{or} or C_{oa} were stated by a calculation according to the standard STN ISO 76.

Basic static load rating is the load which corresponds to calculated contact stresses at the most heavily loaded contact zone of the rolling element and bearing raceway:

- 4 600 MPa for double row self-aligning ball bearings
- 4 200 MPa for the other ball bearings
- 4 000 MPa for cylindrical roller, needle roller, spherical roller and tapered roller bearings

1.2.2 Equivalent Static Load

Equivalent static load is a re-calculated radial load P_{or} for radial bearings and axial axis load P_{oa} for thrust bearings.

$$P_{or} = X_o \cdot F_r + Y_o \cdot F_a$$

$$P_{oa} = X_o \cdot F_r + Y_o \cdot F_a$$

P_{or}	- radial equivalent static load	[kN]
P_{oa}	- axial equivalent static load	[kN]
F_r	- radial load	[kN]
F_a	- axial load	[kN]
X_o	- radial load factor	
Y_o	- axial load factor	

Factor s_0			Table 8
Bearing motion	Type of load, demands on bearing running	s_0 Ball Bearings	s_0 Cylindrical roller, needle roller, spherical roller, tapered roller bearings
Rotary	distinct impact load, high demands on smooth running	2	4
	after static loading bearing rotates under smaller load	1,5	3
	normal demands on smooth running		
	normal operating conditions and normal demands on running	1	1,5
	smooth impact-free operating	0,5	1
Oscillating	small oscillation angle with high frequency, with uneven impact loading	2	3,5
	large oscillating angle with low frequency and with approximately constant periodic load	1,5	2,5
Non-rotary	distinct impact load	1,5 to 1	3 to 2
	normal and small load, no special demands on bearing operation	1 to 0,4	2 to 0,8
	spherical roller thrust bearings at all kinds of motions and loads	-	4

Factors X_o and Y_o are given for individual bearings in the dimension tables of this publication. Subsequently, closer data for stating the equivalent static load of given bearing type are also given here.

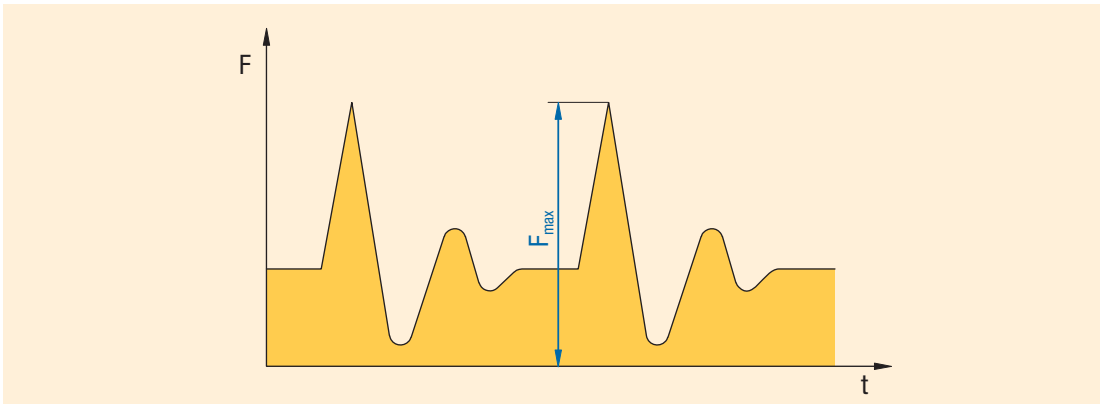
1.2.3 Bearing Safety under Static Load

In practice the bearing safety under static load is found by the ratio C_{or}/P_{or} or C_{oa}/P_{oa} and is compared with data in table 8, where the values of least permissible factors so for various operation conditions are shown.

$$s_o = \frac{C_{or}}{P_{or}} \quad \text{or} \quad \frac{C_{oa}}{P_{oa}}$$

s_o	- safety factor under static load	
C_{or}	- radial basic static load rating	[kN]
C_{oa}	- axial basic static load rating	[kN]
P_{or}	- radial equivalent static load or maximum acting impact force	
	$F_{r \max}$ (Figure 6) under distinct impact load	[kN]
P_{oa}	- axial equivalent static load or maximum acting impact force	
	$F_{a \max}$ (Figure 6) under distinct impact load	[kN]

Figure 6



1.3 LIMITING SPEED

Limiting speed depends on the bearing type, its accuracy, cage design, internal clearance, operating conditions in arrangement, kind of lubrication and on other factors. This influence summary determines the heat generation in the bearing and also limited rotational speed which is first of all limited by the lubricant operating temperature. For orientation, limiting rotational speed values are shown in the dimension tables for individual bearings in normal tolerance class, both for grease and oil lubrication. Given values are valid under presumption of adequate load ($L_{10h} \geq 100\,000$ h), normal operating conditions and cooling.

The influence of larger load is shown mainly with bearings of larger dimension with life $L_{10h} < 100\,000$ h, where it is necessary to consider lowering the value of limiting frequency of rotation. Equally it is necessary to lower the value of limiting frequency for radial bearings, which are constantly loaded with a relatively large axial force. The resulting value of rotation frequency is dependent on the ratio of axial and radial load F_a/F_r . If $F_a/F_r > 0,6$, it is recommended mainly for double row self-aligning ball bearings, spherical bearings and single row taper roller bearings, consult the values of limiting frequency with supplier. The given limiting rotation frequency is possible to cross with ball bearings up to 3 times, cylindrical bearings 2 times, and other bearings other than spherical and tapered roller bearings 1,5 times and for spherical bearings 1,3 times.

This exceeding requires:

- adaptation of lubrication and cooling
- higher bearing tolerance class and corresponding accuracy of the abutment parts
- higher radial clearance than normal
- cage of suitable design and material

In this case it is necessary to consult the bearing use with mentioned special workstations.